NB. These formulae and symbols are for guidance only and other formulae which give equally valid results are acceptable.

$$\begin{split} &\rho = \frac{\text{Mass}}{\text{Volume}} \\ &RD = \frac{\rho_{\text{SUBSTANCE}}}{\rho_{\text{FW}}} \\ &\nabla = (L \times B \times d) \times C_b \\ &\Delta = \nabla \times \rho \\ &DWT = \Delta - \Delta_{\text{LIGHT}} \\ &A_w = (L \times B) \times C_w \\ &TPC = \frac{A_w}{100} \times \rho \\ &Sinkage/Rise = \frac{W}{\text{TPC}} \\ &FWA = \frac{\Delta_{\text{SUMMER}}}{4 \times \text{TPC}_{SW}} \\ &DWA = \frac{(1025 - \rho_{\text{dock}})}{25} \times FWA \\ &MSS = \Delta \times GZ \\ &GZ = GM \times sin\theta \\ &GZ = [GM + \frac{1}{2}BMtan^2\theta]sin\theta \\ &GZ = [GM + \frac{1}{2}BMtan^2\theta]sin\theta \\ &GZ = KN - (KG \times sin\theta) \\ &Dynamic Stability = Area under GZ curve \times \Delta \\ &Area under curve (SR1) = \frac{1}{3} \times h \times (y_1 + 4y_2 + y_3) \\ &Area under curve (SR2) = \frac{3}{8} \times h \times (y_1 + 3y_2 + 3y_3 + y_4) \\ &\lambda_0 = \frac{Total \ VHM}{SF \times \Delta} \\ &\lambda_{40} = \lambda_0 \times 0.8 \\ &Actual \ HM = \frac{Total \ VHM}{SF} \\ &Approx' \ Angle \ of \ Heel = \frac{Actual \ HM}{Max' \ Permissible \ HM} \times 12^\circ \\ &Reduction \ \ in \ GZ = (GG_H \times cos\theta) + (GG_V \times sin\theta) \\ &Rolling \ Period \ T \ (secs) = \frac{2 \times \pi \times K}{\sqrt{g \times GM}} \end{split}$$

$$GG_{\text{H/V}} = \frac{w \times s}{\Lambda}$$

$$FSC = \frac{i}{\Lambda} \times \rho_T$$

$$FSC = \frac{I \times b^3}{12 \times \Delta} \times \rho_{\scriptscriptstyle T}$$

$$FSC = \frac{FSM}{\Delta}$$

$$tan\theta = \frac{GG_{_H}}{GM}$$

$$KG = \frac{\Sigma Moments}{\Sigma Weights}$$

$$GG_{\text{H}} = \frac{\Sigma Moments}{\Sigma Weights}$$

$$GM = \frac{w \times s \times length}{\Delta \times deflection}$$

$$tan \ angle \ of \ Loll = \sqrt{\frac{-2 \times GM}{BM_T}}$$

$$GM \ at \ angle \ of \ Loll = \frac{2 \times initial \ GM}{cos \theta}$$

$$tan\theta = \sqrt[3]{\frac{2\times w\times s}{\Delta\times BM_{_T}}}$$

Draught when heeled =  $(upright draft \times cos\theta) + (\frac{1}{2} \times beam \times sin\theta)$ 

Position of the Metacentre

$$KM_T = KB + BM_T$$

$$BM_T = \frac{I_T}{\nabla}$$

$$BM_{T} (box) = \frac{L \times B^{3}}{12 \times \nabla}$$

Distance Summer LL to Winter LL =  $\frac{1}{48}$  Summer draft

Distance Summer LL to Tropical LL =  $\frac{1}{48}$  Summer draft

$$\begin{split} &\mathsf{KM}_{\bot} = \mathsf{KB} + \mathsf{BM}_{\bot} \\ &\mathsf{BM}_{\bot} = \frac{I_{\bot}}{V} \\ &\mathsf{BM}_{\bot}(\mathsf{box}) = \frac{L^3 \times \mathsf{B}}{12 \times V} \\ &\mathsf{MCTC} = \frac{\Delta \times \mathsf{GM}_{\bot}}{100 \times \mathsf{LBP}} \\ &\mathsf{CoT} = \frac{\Sigma \mathsf{Trimming} \ \mathsf{Moment}}{\mathsf{MCTC}} \\ &\mathsf{Change} \ \mathsf{of} \ \mathsf{trim} \ \mathsf{aft} = \mathsf{change} \ \mathsf{of} \ \mathsf{trim} \times \frac{\mathsf{LCF}}{\mathsf{LBP}} \\ &\mathsf{Change} \ \mathsf{of} \ \mathsf{trim} \ \mathsf{fud} = \mathsf{change} \ \mathsf{of} \ \mathsf{trim} \times \frac{\mathsf{LBP} - \mathsf{LCF}}{\mathsf{LBP}} \\ &\mathsf{True} \ \mathsf{mean} \ \mathsf{draught} = \mathsf{draught} \ \mathsf{aft} \pm \left(\mathsf{trim} \times \frac{\mathsf{LCF}}{\mathsf{LBP}}\right) \\ &\mathsf{Trim} = \frac{\Delta \times (\mathsf{LCG} \sim \mathsf{LCB})}{\mathsf{MCTC}} \\ &\mathsf{P} = \frac{\mathsf{trim} \times \mathsf{MCTC}}{\mathsf{LCF}} \\ &\mathsf{P} = \mathsf{Reduction} \quad \mathsf{in} \ \mathsf{TMD} \ \mathsf{x} \ \mathsf{TPC} \\ &\mathsf{Loss} \ \mathsf{of} \ \mathsf{GM} = \frac{P \times \mathsf{KM}_{\top}}{\Delta} \qquad \mathsf{or} \qquad \frac{P \times \mathsf{KG}}{\Delta - \mathsf{P}} \\ &\mathsf{tan} \ \theta = \frac{v^2 \times \mathsf{BG}}{g \times \mathsf{R} \times \mathsf{GM}} \\ &\mathsf{Permeabili} \ \mathsf{ty} \ (\mu) = \frac{\mathsf{Volume} \ \mathsf{available} \ \mathsf{for} \ \mathsf{Vater}}{\mathsf{Volume} \ \mathsf{available}} \ \mathsf{for} \ \mathsf{Cargo} \times \mathsf{100} \\ &\mathsf{Solid} \ \mathsf{Factor} = \frac{1}{\mathsf{RD}} \\ &\mathsf{Permeabili} \ \mathsf{ty} \ (\mu) = \frac{\mathsf{SF} \ \mathsf{of} \ \mathsf{Cargo} \ \mathsf{-Solid} \ \mathsf{Factor}}{\mathsf{SF} \ \mathsf{of} \ \mathsf{Cargo}} \times \mathsf{100} \\ &\mathsf{Effective} \ \mathsf{length} \ \mathsf{=l}_{\mathsf{I} \times \mathsf{H}} \\ &\mathsf{Sinkage} = \frac{\mathsf{Volume} \ \mathsf{of} \ \mathsf{Bilged} \ \mathsf{Compartmen} \ \mathsf{t} \times \mathsf{Permeabili} \ \mathsf{ty}(\mu)}{\mathsf{Intact} \ \mathsf{Water} \ \mathsf{Plane} \ \mathsf{Area}} \\ &\mathsf{I}_{\mathsf{PARALLEL} \ \mathsf{AXIS}} \ \mathsf{=l}_{\mathsf{CENTROIDAL} \ \mathsf{AXIS}} \ \mathsf{+As}^2} \\ &\mathsf{Tan} \ \theta = \frac{\mathsf{BB}_{\mathsf{H}}}{\mathsf{GM}_{\mathsf{BII} \ \mathsf{GFD}}} \end{aligned}$$

Correction to observed drafts =

$$\frac{I_1}{L_1} \times Trim$$

Midships draft corrected for deflection =

$$\frac{d_{\text{FP}} + \left(6 \times d_{\text{M}}\right) + d_{\text{AP}}}{8}$$

Correction of Midships draft to True Mean Draft when CF not midships =

Distance of CF from Midships × Trim (True Trim at Perp's)

LBP

Second Trim Correction for position of CF if trimmed hydrostatics are not supplied (form correction) =

$$\frac{\text{True Trim} \times (\text{MCTC}_2 - \text{MCTC}_1)}{2 \times \text{TPC} \times \text{LBP}}$$

Alternative form Correction =

$$\frac{50 \times \text{True Trim}^2 \times (\text{MCTC}_2 - \text{MCTC}_1)}{\text{LBP}}$$